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### What is a fitting?

- AWWA M11
- AWWA C208
- ASME BPVC



$$t = \frac{P_w D_o}{2 S}$$

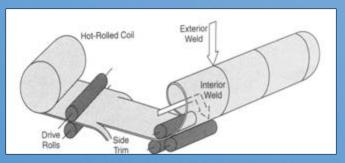
- t Required thickness of steel
- Pw Working pressure
- D<sub>o</sub> Outside diameter of pipe
- S Limited to 50% of the min. yield strength of steel



# Steel Water Pipe Fittings – Design Helical Forming and Weld Machine







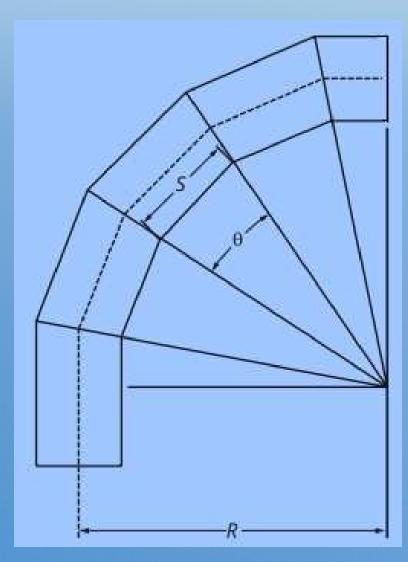




Elbows/Bends

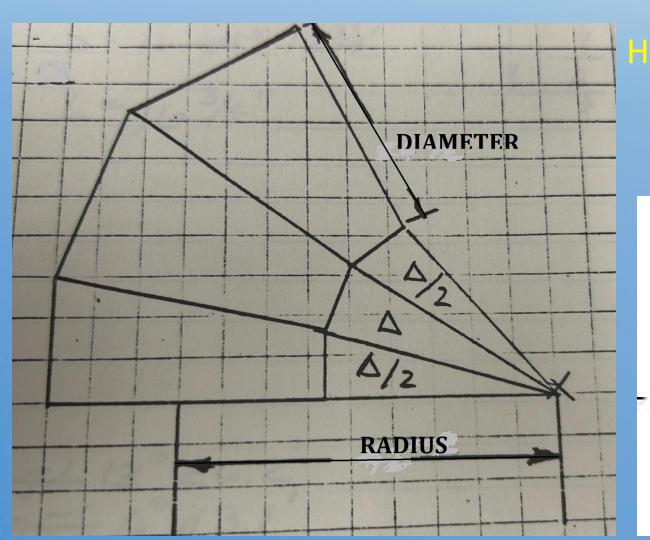




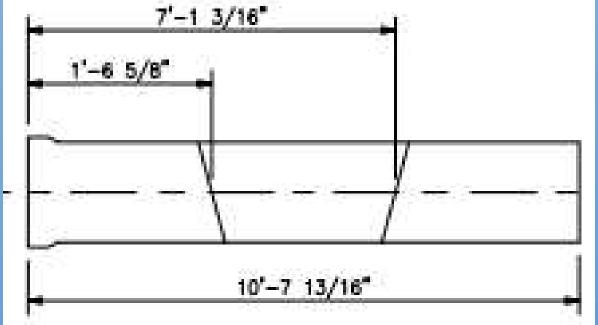


Elbow Leg Lay Length

At 90°, LL = R



How many segments will an elbow have?





 $T_{\nu}$  - Required steel thickness

R - Elbow Radius

D - Outside diameter of pipe

p - internal design pressure

σ - allowable design stress

Cylinder Thickness for bends < 2.5 x D

$$T_y = \frac{pD}{2\sigma} \left(1 + \frac{D}{3R - 1.5D}\right)$$



- A Required elbow angle
- R Elbow Radius
- D Outside diameter of pipe
- p internal design pressure
- σ allowable design stress

Example: 48" OD x 90° Elbow with a standard radius (1 x D) at 150psi, 36ksi steel

$$T_y = \frac{pD}{2\sigma} (1 + \frac{D}{3R-1.5D})$$



- Required elbow angle
- R Elbow Radius
- D Outside diameter of pipe
- p internal design pressure
- σ allowable design stress

Example: 48" Dia x 90° Elbow with a standard radius (1 x D) at 150psi, 36ksi steel

$$T_y = \frac{150 \times 48}{2 \times 18,000} \left(1 + \frac{48}{3(48) - 1.5(48)}\right)$$

$$T_{y} = 0.333$$
"

>> BXS >>

0+43.88

```
C = Manufactured angle of elbow (deflection angle in plane of elbow)

H = Horizontal projection of deflection angle of bend

V = Vertical angle of approaching line (near end) with horizontal plane

V'= Vertical angle of departing line (far end) with horizontal plane
```

Compound bend formula

Cos C = (CosH CosV CosV') + (SinV SinV')

>> BXS >>

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Compound bend formula

Cos C = (CosH CosV CosV) + (SinV SinV)





Reducer Lay Length

$$LL = 4 \times (D_L - D_S)$$









Tees, Outlets & Laterals

$$PDV = \frac{\text{Kpd}^2}{D_o(\sin^2 \Delta)}$$

K = 1.0 except for full-size cross(1.5)

p = design pressure, psi

d = outlet outside diameter, in.

D<sub>o</sub> = main pipe outside diameter, in.

△ = outlet angle of deflection, degrees



$$PDV = \frac{\text{Kpd}_0^2}{D_0 \left(\sin^2 \Delta\right)}$$

K = 1.0 except for full-size cross(1.5)

p = design pressure, psi

do = outlet outside diameter, in.

Do = main pipe outside diameter, in.

a = outlet angle of deflection, degrees



$$PDV = \frac{\text{Kpd}^2}{D_o(\sin^2 \Delta)}$$

Example: 48" x 8" outlet at 150psi

K = 1.0

**p** = 150 psi

do = 8.625 in.

Do = 49.75 in.

 $T_{y} = 0.375$ "

△ = radial or 90 degrees



Example: 48" x 8" outlet at 150psi

PDV =  $1.0(150)(8.625)^2$ 49.75 (sin<sup>2</sup> 90)

PDV = 299





$$PDV = \frac{\text{Kpd}^2}{D_o(\sin^2 \Delta)}$$

PDV	Reinforcement		
< 6,000	С		
6,000-9,000	ICT, W, or C $(M = 0.000167xPDV)$		
> 9,000	Crotch Plate		

Allowable stress,  $\sigma = 0.5 \times Pw \text{ or } 0.75 \times Pw + Pt \text{ or } :P_{ft}$ 

#### Input variables

 $D_n = run pipe OD, in.$ 

Ty = run cylinder thickness, in.

 $d_0$  = outlet pipe OD, in.

t<sub>v</sub> = outlet cylinder thickness, in.

 $\Delta$  = outlet deflection angle, degrees

#### Output variables

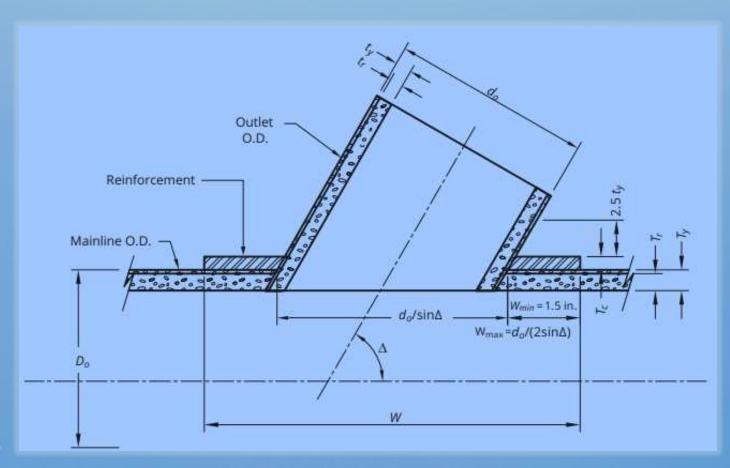
t<sub>r</sub> = required outlet cyl thickness, in.

Tr = required run cyl thickness, in.

Tc = collar or wrapper thickness, in.

w = collar or wrapper edge width, in.

W = overall collar or wrapper width, in.



√ Theoretical cyl thickness of run pipe

✓ Theoretical cyl thickness of branch

Theoretical reinforcement area

✓ Available reinforcement

Required Reinforcement

$$Tr = \frac{pD_o}{2\sigma}$$

$$t_r = \frac{pd_o}{2\sigma}$$

$$A_r = M[Tr(\frac{d_o - 2ty}{\sin \Delta^\circ})]$$

$$A_{a} = \frac{d_{o}-2ty}{\sin \Delta} (T_{y}-T_{r}) + 5t_{y} (t_{y}-t_{r})s_{r1}$$

$$= \frac{A_r - A_u}{S_{r2}}$$

✓ Theoretical cyl thickness of run pipe

$$T_T = \frac{pD_o}{2\sigma} = \frac{150(49.75)}{2(18,000)} = 0.207$$

✓ Theoretical cyl thickness of branch

$$t_r = \frac{pd_o}{2\sigma} = \frac{150(8.625)}{2(17,500)} = 0.037$$
"

Theoretical reinforcement area

$$A_r = M[Tr(\frac{d_o - 2ty}{\sin \Delta^\circ})]$$

$$=1[0.207(\frac{8.625-2(0.322")}{\sin 90^{\circ}})]=1.656in^{2}$$

$$A_{a} = \frac{D_{o} - 2ty}{\sin A} (T_{y} - T_{r}) + 5t_{y} (t_{y} - t_{r}) s_{r1}$$

$$A_a = 8 (0.375"-0.207") + 5(0.322")(.322-.037)0.972$$
  
= 1.79 $in^2$ 

$$A_{w} = \frac{A_{r} - A_{u}}{S_{r2}} = \frac{1.656 - 1.79}{1} = -0.134in^{2}$$

$$w = \frac{d_o}{2\sin \Delta} = \frac{8.625}{2\sin 90^\circ} = 4.312in$$

$$T_c = \frac{A_w}{2w} = \frac{0.986}{2(4.312)} = 0.114in \text{ round up to } 0.125''$$

Min Reinforcement Width 
$$w = \frac{A_w}{2T_c} = \frac{0.986}{2(.125'')} = 3.94in$$

Overall Reinforcement Width 
$$W = 2w + \frac{cl_o}{sin\Delta} = 2(3.94) + \frac{8.625}{1} = 16.5in$$

#### Outlet Reinforcement Design Calculation

Per AWWA Manual M11 (5th Edition) - Chapter 7 48" Main Line with 8" Radial Branch

Mainline Pipe					
Nominal diameter:	48	in			
Cylinder outside diameter:	49.75	in	D		
Cylinder thickness:	0.375	in	$T_{\nu}$		
Material minimum yield:	36,000	psi			
Branch Pipe					
Nominal diameter:		in			
Cylinder outside diameter:	8.625		d		
Cylinder Thickness:	0.322	in	$t_{\nu}$		
Material minimum yield:	35,000	psi	,		
Branch type:	Radial				
Deflection angle:	90	degrees	Δ		
Branch configuration:	Single				
Reinforcement material minimum yield:	36,000	poi.			
Design pressure:	200		P		
Doorgi i procedio.	200	ро,	•		
Outlet type multiplier:	1.0		K		
Branch pipe strength reduction factor:	0.972		57' /		
Reinforcement strength reduction factor:	1.000		57° 2		
Pressure Diameter Value	299		PDV		
Fressure Diameter Value	0.17		d/D		
	0.11		42		
Reinforcement type:	Collar				
Multiplier Factor:	1.000		M-factor		
Required mainline cylinder thickness:	0.276	in	$T_r$		
Required branch cylinder thickness:	0.049	in	$t_r$		
Theoretical reinforcement area:	2.203	in²	$A_r$		
Run pipe excess area:	0.79	in²	$A_{I}$		
Branch pipe excess area:	0.427	in²	$A_2$		
Area available:	1.217	in²	$A_a = A_1 + A_2$		
Additional reinforcement area required:	0.986	in²	$A_w = A_r - A_a$		
Minimum reinforcement thickness:	0.114	in	T(min)		
Minimum allowable width:	1.50		w (min)		
Vidth based on reinforcement thickness:	2.63		w (use)		
Maximum allowable width:	4.31	ın	w (max)		

3/16" THICK BY 14.00" LONG BY 14.00" CIRCUMFERENTIAL WIDTH COLLAR Note: Required width/length dimensions rounded up to the nearest 1/4"



#### Steel Water Pipe Fittings – Design



3/16" x 14" long x 14" wide

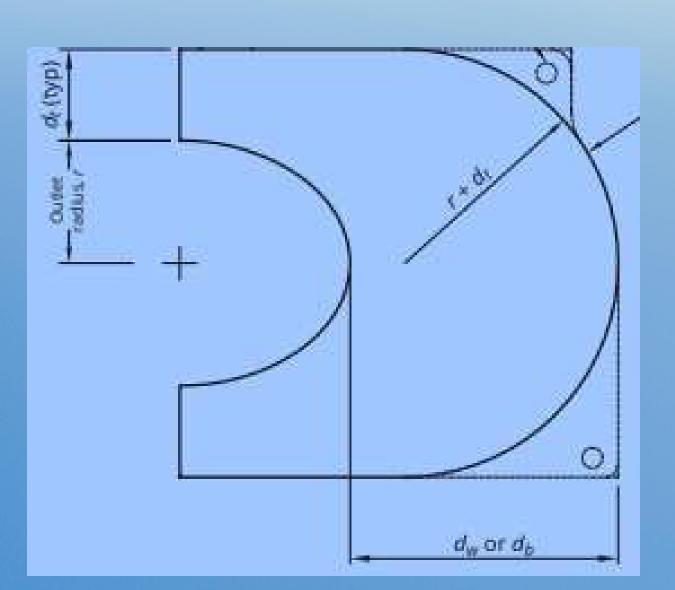








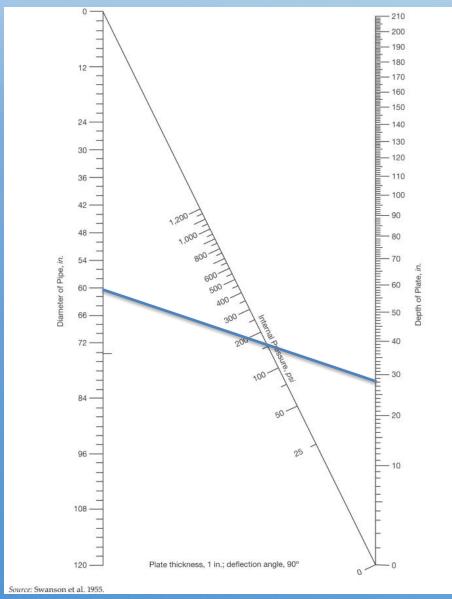
CROTCH PLATES



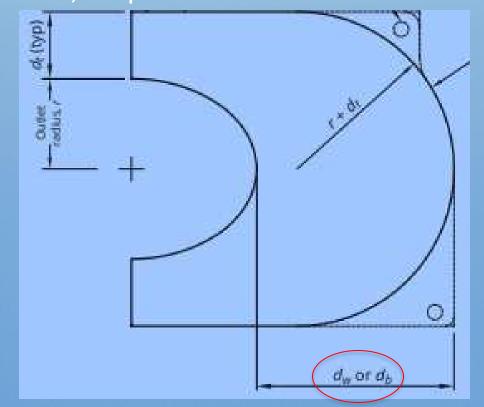
 $d_w$  and  $d_b$  = depth of plate

d<sub>t</sub> = depth of plate between branch and mainline cylinder

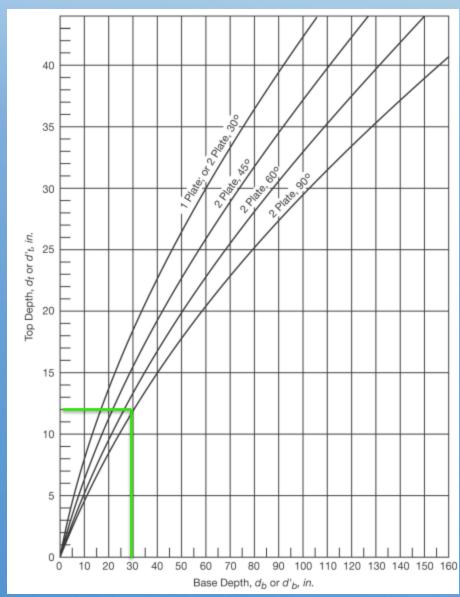
t = crotch plate thickness



Dia, D = 60 in, size-on-size tee, at 150psi  $\sigma = 36,000$ psi

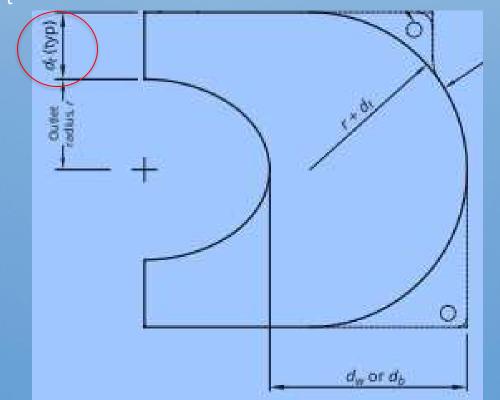


30/36 = 0.83" thick plate and from nomograph, depth of plate is 29in



Dia, D = 60 in, size-on-size, at 150psi  $\sigma$  = 36,000psi

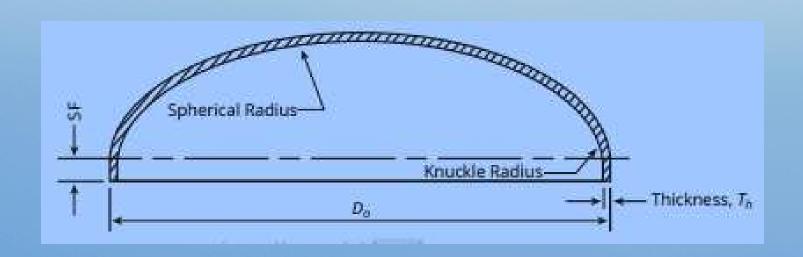
depth of plate,  $d_b$  is 29in, using this nomograph,  $d_t = 12$ ".



#### Bulkheads







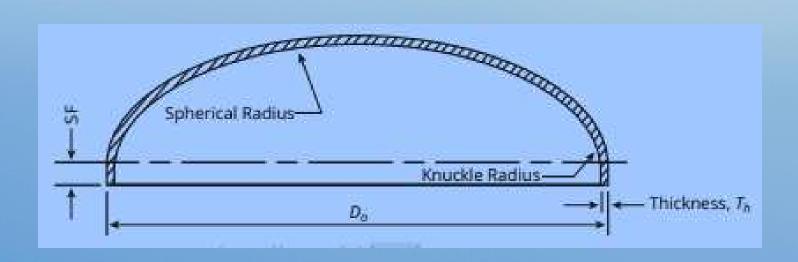
 $T_h$  = min req'd thickness of head

p = design pressure, psi

 $D_h$  = dished head outside diameter, in.

σ = allowable design stress for dish, psi

$$T_h = \frac{pD_h}{2\sigma - 0.2p}$$



$$T_h = \frac{pD_h}{2\sigma - 0.2p}$$

 $T_h$  = min req'd thickness of head

p = 150 psi

 $D_h = 49.75 in.$ 

 $\sigma$  = 0.5 x 38,000psi

$$= \frac{150 \times 49.75}{2(19,000) - 0.2(150)}$$

$$= 0.197in$$

What else? What other fittings are there?

Questions?

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